

No. 10-02-01-24R/01

SUBSYSTEM: Noz ASSEMBLY: Noz FMEA ITEM NO.: 10-0 CIL REV NO.: M (E DATE: 10 A SUPERSEDES PAGE: 331- DATED: 31 J		I: Noz Noz NO.: 10-0 : M (E 10 A ES PAGE: 331 31 J T: B. A BY:	ul 2000 . Frandsen : <u>K. G. Sanofsky</u>	CRITICALITY C PART NO.: PHASE(S): QUANTITY: EFFECTIVITY: HAZARD REF.: DATE: 10 Apr 2002	Nose Inlet-to-Throat Joint, Primary O-ring, Secondary O-ring (2) (See Section 6.0) Boost(BT) (See Section 6.0) (See Table 101-6)	
1.0	FAILUR	E CONDITION:	Failure during operation (D)			
2.0	FAILUR	E MODE:	1.0 Leakage of primary O-ring	and secondary (D-ring	
3.0	FAILUR	E EFFECTS:	Failure could result in hot gas flowing through joint resulting in a causing loss of nozzle, thrust imbalance between SRBs, causing RSRM, crew, and vehicle			
4.0	FAILUR	E CAUSES (FC)	:			
	FC NO.	DESCRIPTION			FAILURE CAUSE KEY	
	1.1	Nonconforming	O-ring splice or repair		Α	
	1.2	Nonconforming	O-ring dimensions		В	
	1.3	O-ring cut or da	amaged		С	
	1.4	Nonconforming	O-ring voids, inclusions, or sub	surface indication	ns D	
	1.5	Age degradatio	n of O-ring		Е	
	1.6	Moisture and/or	fungus degradation of O-ring		F	
	1.7	O-ring gland do	es not meet dimensional or sur	face finish require	ements G	
	1.8	O-ring imprope	rly installed		Н	
	1.9	Transportation,	handling, or assembly damage	:	I	
	1.10	Sealing surface	es contamination or corrosion		J	
	1.11	Nonconforming	physical or mechanical properties		K	



DATE: 10 Apr 2002 No. 10-02-01-24R/01 SUPERSEDES PAGE: 331-1ff. DATED: 31 Jul 2000

5.0 REDUNDANCY SCREENS:

SCREEN A: Pass--The leak test procedure verifies the primary O-ring and secondary O-ring seals.

SCREEN B: Fail--No provision is made for failure detection by the crew.

SCREEN C: Fail--The primary and secondary O-ring seal can be lost due to a single credible cause such as a

surface defect on the sealing surface.

1. The primary O-ring and secondary O-ring form part of a redundant seal system at the nose inlet-to-throat joint when the leak check port O-ring seals. The secondary O-ring will see no pressure unless the primary O-ring fails. If the primary O-ring fails, the secondary O-ring will be pressurized and still maintain a seal. If both the primary O-ring and secondary O-ring fail, a leak path will exist and could result in loss of crew and mission.

6.0 ITEM DESCRIPTION:

The Nose Inlet-to-Throat Nozzle Joint has a primary O-ring and a secondary O-ring (Figures 1 and 2).
 The assembled joint is per engineering drawings. Materials are listed in Table 1.

Table 1. MATERIALS

Drawing No.	Name	Material	Specification	Quantity
1U79146 1U75150 1U75547	Nose-Throat Assembly, Nozzle Packing, Preformed Fluorocarbon Housing, Throat Support, Nozzle	Black Fluorocarbon Rubber	STW4-3339	1/motor 1/motor 1/motor
1U75398	Housing Assembly-Nose/Inlet, Nozzle Corrosion-Preventive Compound and O-ring Lubricant	Heavy-Duty Calcium Grease	STW5-2942	1/motor A/R
1U51916	Cartridge Assembly	Heavy-Duty Calcium Grease, Filtered and Placed in an Application Cartridge	STW7-3657	A/R

6.1 CHARACTERISTICS:

- 1. The Nose Inlet-to-Throat Joint allows the Nose Inlet Housing Assembly to be mounted to the Nozzle Housing Throat Support. The unit is assembled with O-rings and bolts to assure there is no leakage.
- The seals at the Nose Inlet-to-Throat Joint are designed so that the O-ring maintains constant contact with its cavity at all times. Squeeze, fill, and tracking are taken into account, relating to O-ring groove tolerance.
- 3. The O-ring is a one-time-use item.
- 4. The joint and seals are an important part of the assembled rocket motor case. The assembled RSRM is a combustion chamber made up of segments and the nozzle, sealed with O-rings, that must contain and direct pressure generated by burning propellant.

7.0 FAILURE HISTORY/RELATED EXPERIENCE:

 Current data on test failures, flight failures, unexplained failures, and other failures during RSRM ground processing activity can be found in the PRACA database.

8.0 OPERATIONAL USE: N/A



No. 10-02-01-24R/01

DATE: 10 Apr 2002 SUPERSEDES PAGE: 331-1ff. DATED: 31 Jul 2000

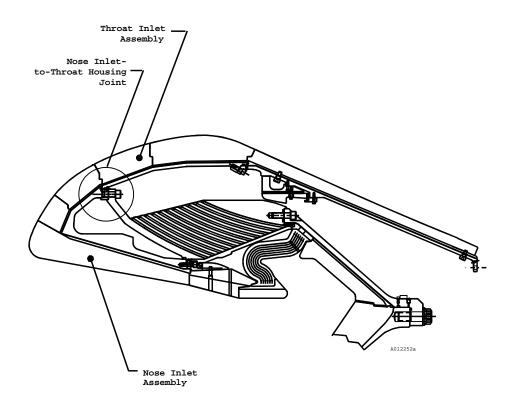


Figure 1. Nose Inlet-to-Throat Joint Location



No. 10-02-01-24R/01

DATE: 10 Apr 2002 SUPERSEDES PAGE: 331-1ff. DATED: 31 Jul 2000

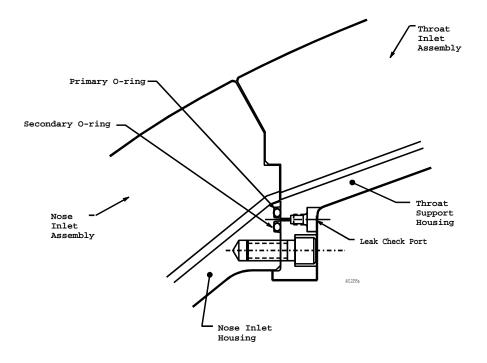


Figure 2. Nose Inlet-to-Throat Joint



DATE: 10 Apr 2002 No. 10-02-01-24R/01 SUPERSEDES PAGE: 331-1ff. DATED: 31 Jul 2000

9.0 RATIONALE FOR RETENTION:

9.1 DESIGN:

DCN FAILURE CAUSES

<u>CN</u>	FAILURE CAUSES		
	Α	1.	Large O-rings are per engineering that covers process controls for fabrication of spliced joints and repairs.
	A	2.	Splice joints are cut on an angle and bonded together in a mold (using 100 percent of the scarf area) using an adhesive with the same physical and chemical properties as the parent stock.
	A,D	3.	O-rings were tested to determine size and types of flaws that could cause sealing problems per TWR-17750.
	В	4.	Criteria for O-ring dimensions are per TWR-15771.
	В	5.	Both O-ring designs provide constant contact between O-ring and mating sealing surfaces.
	B,D	6.	Large O-rings are per engineering that establishes geometric dimensions, design requirements, and fabrication details.
	C,H	7.	Large O-rings are individually packaged per engineering.
	C,H	8.	Large O-ring design allows for a minimum of stretching without damage to the O-ring. Proper installation without over stretching is per engineering.
	C,H	9.	Material selection for the O-rings was based in part on resistance to damage per TWR-17082.
	C,H	10.	Design development testing of O-ring twisting and its effect on performance is per ETP-0153 and TWR-17991.
	E	11.	Fluorocarbon rubber O-rings are suitable for periods of storage of up to 20 years (O-ring Handbook, ORD 5700, Copyright 1982, by Parker Seal Group, Lexington, KY). Environment and age are significant to useful seal life, both in storage and actual service.
	E		 O-rings are packaged and stored to preclude deterioration caused by ozone, grease, ultraviolet light, and excessive temperature.
	E	12.	Large O-ring time duration of supplier storage and total shelf life prior to installation is per engineering.
	E	13.	Aging studies of O-rings after 5 years installation life were performed. Test results are applicable to all RSRM fluorocarbon seals. Fluorocarbon maintained its tracking ability and resiliency. Fluorocarbon was certified to maintain its sealing capability over 5 years per TWR-65546.
	E	14.	The O-ring is a one-time-use item.
	E	15.	Grease is stored at warehouse-ambient condition that is any condition of temperature and relative humidity experienced by the material when stored in an enclosed warehouse, in unopened containers or containers that were resealed after each use. Storage life under these conditions is per engineering.

REVISION M	(DCN-533)
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CRITICAL ITEMS LIST (CIL)					
		No. 10-02-01-24R/01	DATE: SUPERSEDES PAGE: DATED:	10 Apr 2002 331-1ff. 31 Jul 2000	
Е	16.	Aging studies to demonstrate characteristics of grewere performed on TEM-9. Results showed to corrosion protection for D6AC steel, and that all claremained intact per TWR-61408 and TWR-64397.	hat grease provide	d adequate	
E	17.	Large O-rings and filtered grease are included in th	e aft segment life ve	rification.	
F,K	18.	Large O-rings are high-temperature, low-comprefluorocarbon rubber.	ession set, fluid-res	istant, black	
F	19.	O-ring swell is negligible unless the O-ring und immersion (O-ring Handbook, ORD 5700, Copyrig Lexington, KY).			
F	20.	Fluorocarbon rubber is a non-nutrient to fungus 5700, Copyright 1982, by Parker Seal Group, Lexin		dbook, ORD	
F	21.	Large O-rings are kept dry and clean prior to packa	ging.		
G	22.	O-ring gland design is per engineering drawing determined by Thiokol Design Engineering calc tracking per TWR-15771.			
G	23.	Design verification analysis of data from live firing 17563 shows that O-ring sealing surfaces are acce 09.			
G	24.	Sealing surface requirements during refurbishment	are per engineering	drawings.	
1	25.	Transportation and handling of the nozzle assembly	y items by Thiokol is	per IHM 29.	
1	26.	The RSRM and its component parts, when protect 11325, are capable of being handled and transpears to and from fabrication, test, operational larefurbishment sites.	ported by rail or of	her suitable	
1	27.	Positive cradling or support devices and tie down weight, and contour of components to be trans RSRM segments and other components. Shock devices are used on trucks and dollies to move sen	ported are provided mounting and other	to support er protective	
1	28.	Support equipment used to test, handle, transport the RSRM is certified and verified per TWR-15723.		disassemble	
I	29.	Analysis is conducted by Thiokol engineering to a response of the RSRM nozzle during transportatio launch sites per TWR-16975.			
1	30.	The nozzle assembly is shipped in the aft segment and vibration levels are monitored per engineering by analysis. Monitoring records are evaluated vibration levels per MSFC Specification SE-019-04 16975 documents compliance of the nozzle Specifications.	and applicable loads by Thiokol to verify 9-2H were not excee	s are derived shock and eded. TWR-	
J	31.	Filtered grease is applied to sealing surfaces of t final assembly processes.	he nose throat asse	embly during	

DOC NO. TWR-15712 | VOL III | SEC | 331 | PAGE | 6



			CRITICAL ITEMS LIST (CIL)		
			No. 10-02-01-24R/01	DATE: SUPERSEDES PAGE: DATED:	10 Apr 2002 331-1ff. 31 Jul 2000
	J	32.	Filtered grease filtering is per engineering to control	I contamination.	
	J	33.	3. Removal of surface contamination or corrosion is a standard shop whenever contamination or corrosion is noted.		ractice used
	J	34.	34. Contamination control requirements and procedures are per TWR-16564.35. Filtered grease is specified for the nose throat assembly and conforms to marequirements per engineering.		64.
	К	35.			s to material
	Κ	36. Temperature prior to launch is monitored for the nozzle flexible bearing case-to-nozzle joint, and is maintained per TWR-15832. The nose inletjoint is within the temperature maintained area and will benefit from tem conditioning. Joint thermal analysis (O-ring resiliency testing) is per ETP-0 TWR-18597.		nlet-to-throat temperature	
	H,I	37.	Analysis of carbon-cloth phenolic ply angle change Results show that redesigned nozzle phenolic coplane fiber strain and wedge-out potential per TW driven by the Performance Enhancement (PE) Pro 73984. No significant effects on the performance dentified due to PE.	omponents have a 'R-16975. New load ogram were address	reduced in- ds that were sed in TWR-
533	H,I	38.	Thermal analysis per TWR-17219 shows the nozzle performance factor equation based on the remainin phase is complete. This performance factor will be safety factor of 1.4 for the nose inlet assembly and 74238 and TWR-75135. (Carbon phenolic-to-glass and metal housing temperatures were all taken into performance factor will insure that the CEI requirem that the bond between carbon and glass will not except the performance of the performance factor will insure that the CEI requirement that the bond between carbon and glass will not except glass-to-metal remains at ambient temperature during will not be heat affected at splashdown.	g virgin material after equal to or greater the throat assembly interface, bondline to consideration). The ments will be met white deed 600 degree F,	er boost han a per TWR- emperature new ch requires bondline of



10 Apr 2002 DATE: No. 10-02-01-24R/01 SUPERSEDES PAGE: 331-1ff.

DATED: 31 Jul 2000

9.2 TEST AND INSPECTION:

FAILURE CAUSES and DCN TESTS (T)

CIL CODE

1. For New Large O-ring verify:

Α	a.	Diameter	AEB026,AEB027
A	b.	Splice is bonded over 100 percent of the scarf	,
A	C.	No more than five splices	AEB167,AEB169
A	d.	Repairs	AEB265,AEB266
A	е.	Adhesive is made from fluorocarbon rubber	AEB308,AEB311
A	f.	Splice bond integrity	AEB317,AEB319
A,D (T)	g.	Subsurface indications	AEB354
A,C,D,F,H	ĥ.	Surface quality	AEB388,AEB389
A,K (T)	i.	Tensile strength	AEB401,AEB402
A,K (T)	į.	Ultimate elongation	AEB442,AEB443
B	k.	Diameter	AEB014,AEB015,AEB018,AEB023
В	I.	Correct identification	AEB087,AEB100
C,E,F,H	m.	Packaging for damage or violation	AEB179
E,F,K	n.	Material is fluorocarbon rubber	AEB141,AEB151
C,E,F	0.	Packaging is free of staples or other objects	LAA054
F	p.	Clean and dry when packaged	AEB031,AEB034
K (T)	q.	Tensile strength	AEB394,AEB396
K (T)	r.	Ultimate elongation	AGW075,AGM408
K (T)	S.	Compression set	AKW006,AKW011
K (T)	t.	Shore A hardness	AGM304,AGM312

For New Nose-Throat Assembly, Nozzle verify:

A,B,C,D,				
G,H,I,J	(T)	a.	Joint seals are pressure tested	ADN063
Н		b.	Correct identification of primary and secondary O-ring at time of	
			installation	ADN029
C,H		C.	Installation and fit of primary O-ring	ADN042
C,H		d.	Installation and fit of secondary O-ring	ADN097
C,H		e.	Application of filtered grease to secondary O-ring, prior to assembly	ADN010
C,H		f.	Application of filtered grease to primary O-ring, prior to assembly	ADN011
C,H,J		g.	Application of filtered grease to Housing Assembly-Nose/Inlet,	
			Nozzle forward end O-ring grooves prior to assembly	ADN012
C,H,J		h.	Application of filtered grease to Housing-Throat Support, Nozzle	
			forward end sealing surfaces	ADN013
C,H		i.	Secondary O-ring is free from damage prior to installation	ADN074
C,H		j.	Primary and secondary O-ring are unpackaged, processed, and	
			installed one at a time	ADN079
C,H		k.	Primary O-ring is free from damage prior to installation	ADN088
C,H		I.	Condition of primary O-ring after installation into O-ring groove	ADN098
C,H		m.	Condition of secondary O-ring after installation into O-ring groove	LAA125
E		n.	Shelf life compliance of primary O-ring	ADN095
Е		0.	Shelf life compliance of secondary O-ring	ADN104
E		p.	Shelf life of the filtered grease has not been exceeded prior to use	LAA120
E E		q.	Primary O-ring packaging for damage at time of installation	LAA126
E		r.	Secondary O-ring packaging for damage at time of installation	LAA127
F		S.	Housing Assembly-Nose/Inlet, Nozzle forward end primary O-ring	
			groove is free from fungus prior to installation	ADN076
F		t.	Housing Assembly-Nose/Inlet, Nozzle forward end secondary O-	
			ring groove is free from fungus prior to installation	ADN076A
F		u.	Secondary O-ring is free from fungus prior to installation	ADN080

REVISION M (DCN-533)

VOL III DOC NO. SEC PAGE 331 8



				No. 10-02-01-24R/01	DATE: SUPERSEDES PAG DATED:	10 Apr 2002 E: 331-1ff. 31 Jul 2000
F F F			V. W. X. y.	Primary O-ring is free from fungus prior to ins Secondary O-ring is free from moisture prior Primary O-ring is free from moisture prior to i Housing Assembly-Nose/Inlet, Nozzle forwar	to installation nstallation	ADN080A ADN081 ADN081A
F			Z.	groove is free from moisture prior to installati Housing Assembly-Nose/Inlet, Nozzle forwar	on	ADN082
·			aa.	ring groove is free from moisture prior to inst Housing Assembly-Nose/Inlet, Nozzle forwar	allation	ADN082A
				grooves are free from damage prior to install	ation of O-ring	ADN075
			ab.	Housing-Throat Support, Nozzle forward end surfaces are free from damage prior to asser	mbly	ADN103
J			ac.	Housing Assembly-Nose/Inlet, Nozzle forwar grooves are free from corrosion and contami		
J			ad.	assembly Housing-Throat Support, Nozzle forward end	sealing surface is	ADN073
				free from corrosion and contamination prior t		ADN123
		3.	For	New Filtered Grease verify:		
E,F,J,K E,F,J,K E,F,J,K	(T)		a. b. c.	Grease is received from storage unopened of Shelf life of the grease, prior to filtering Contamination	r resealed	ACP015 AMB018L ANO064
E,F,J,K E,F,J,K	(-)		d. e.	Grease conforms to specification Cartridge conforms to drawing		LAA044 LAA046
E,F,J,K			f.	Filtered grease is capped and sealed after fil		LAA047
E,F,J,K			g.	Filtered grease is sent to storage capped and and resealed)	sealed (recapped	LAA063
		4.	For	New Grease verify:		
E,F,J E,F,K E K K K	(T) (T) (T)		a. b. c. d. e. f.	Material received in closed containers Type No shipping or handling damage Penetration Dropping point Zinc concentration		ANO015 ANO050 ANO058 LAA037 ANO042 LAA038
		5.	For	New Housing Assembly-Nose/Inlet, Nozzle ve	rify:	
G G G			a. b. c. d.	O-ring groove diametric location O-ring groove surface finish	AFE088,AFE088A,AFE0 AFE090,AFE090A,AFE0 AFE092,AFE092A,AFE0 AFE095,AFE095A,AFE0	091,AFE091A 093,AFE093A
		6.	For	Refurbished Housing Assembly-Nose/Inlet No	zzle verify:	
G			a.	Surface finish and surface condition		AFE148
		7.	For	New Housing, Throat Support, Nozzle verify:		
G			a.	Surface finish	AFI	N145,AFN146
		8.	For	Refurbished Housing, Throat Support, Nozzle	verify:	
G			a.	Surface finish		AFN004
		10.	KSC	verifies:		

REVISION M (DCN-533)



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CRITICAL ITEMS LIST (CIL)

10 Apr 2002 DATE: No. 10-02-01-24R/01 SUPERSEDES PAGE: 331-1ff.

31 Jul 2000 DATED:

life requirements for the expected launch schedule are met per OMRSD File II, Vol III, C00CA0.030. OMD019

> VOL III TWR-15712 DOC NO. SEC PAGE 331 10